

# LECTURE 1: ELASTIC BEHAVIOR & PROPERTIES OF MATERIALS

## *Learning Outcomes:*

You should be able to:

- Describe how a material responds to an applied load
- Define elastic modulus
- List examples of applications in which elastic modulus is a design criterion.
- Calculate from a given selection the best material for elastic-limited design

# Brief Introduction

- Materials are subjected to forces or loads.

e.g. Al alloy in airplane wing; steel in automobile axle

- Mechanical behavior of materials reflects the relationship between its response or deformation to an applied load or force
- **Factor to consider in design** → nature of applied load, duration, environmental conditions
- **Stress states** → tensile, compressive, bending or shear → constant or fluctuate continuously with time

# Mechanical Properties: Definition

- **Ductility** – ability to deform without fracture
- **Malleability** – ability to withstand deformation under compression without rupture
- **Toughness** – resistance to crack propagation
- **Hardness** – resistance to indentation
- **Stiffness** – resistance of bonds to deform
- **Strength** – resistance to permanent deformation

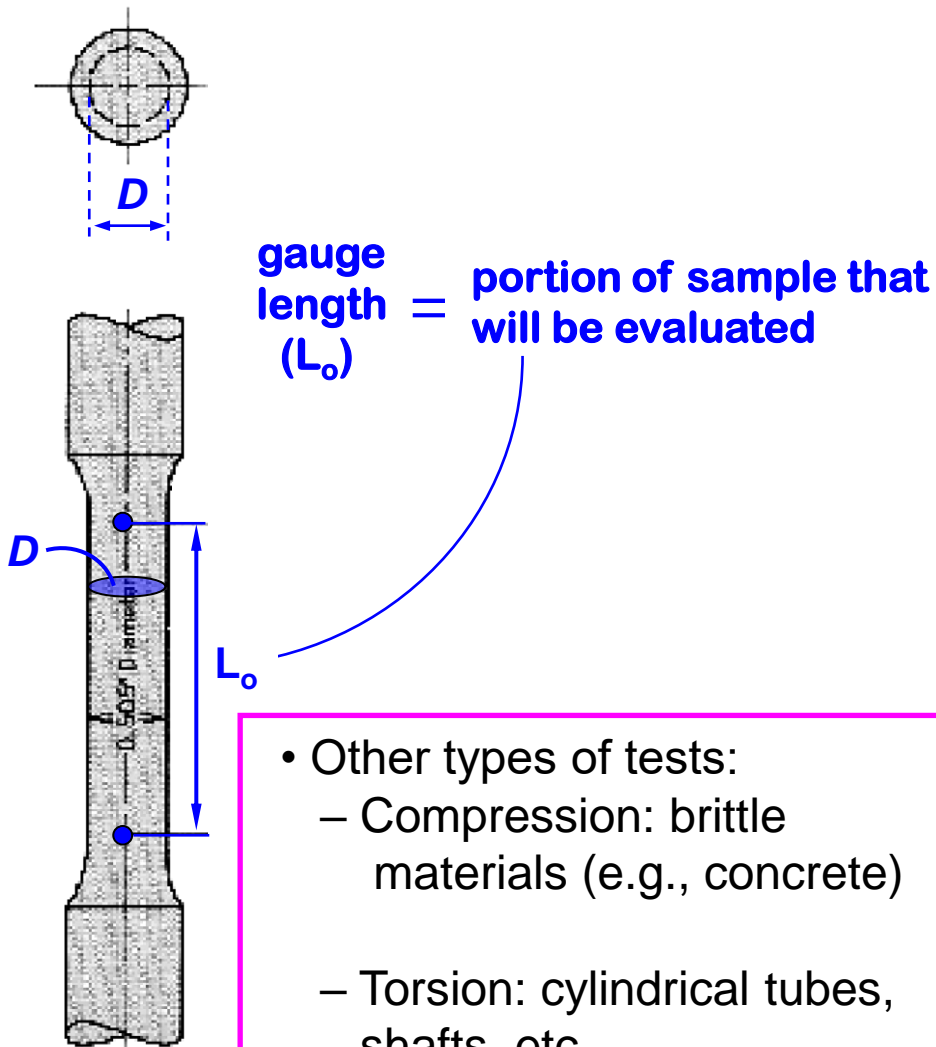
## Definition of Stress and Strain

**(a) Tensile stress** produces an elongation and +ve linear strain

**(b) Compressive strain** produces contraction and –ve linear strain

# Stress-Strain Testing

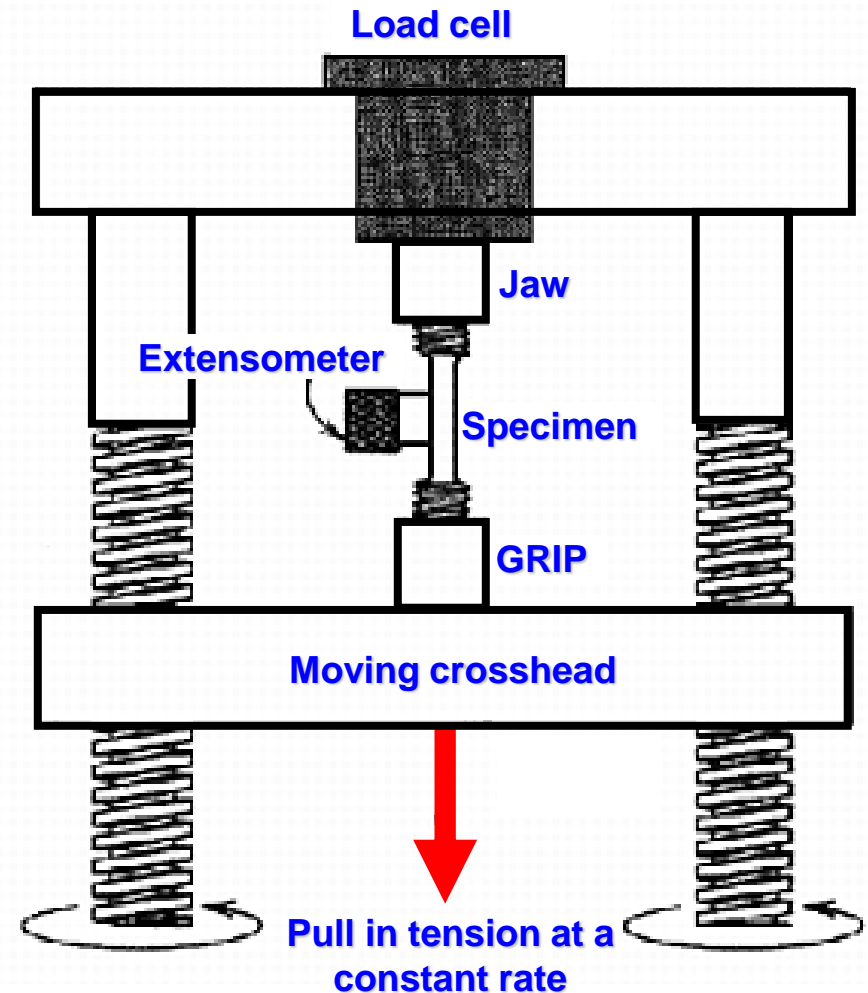
- Typical tensile specimen



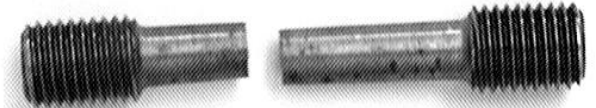
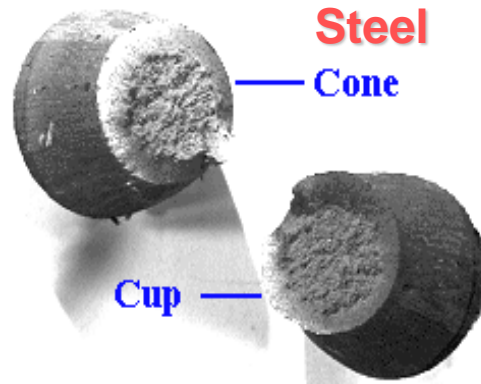
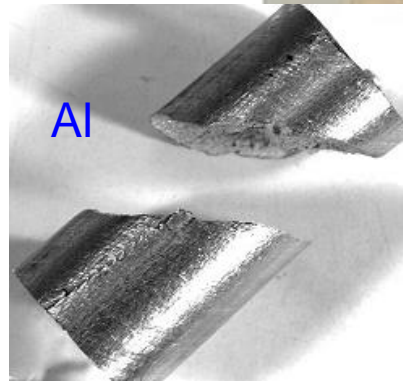
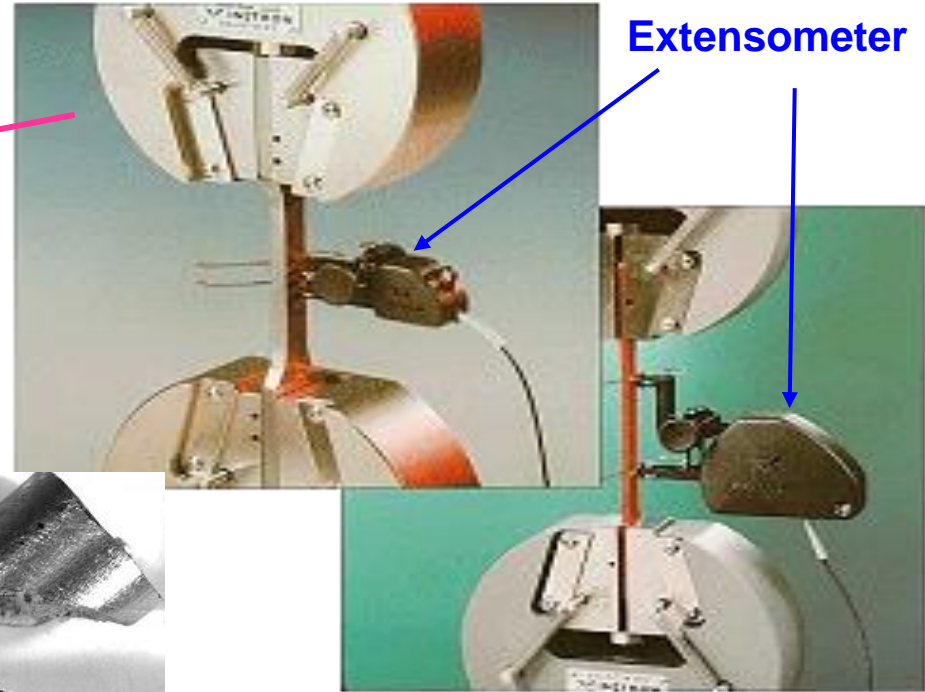
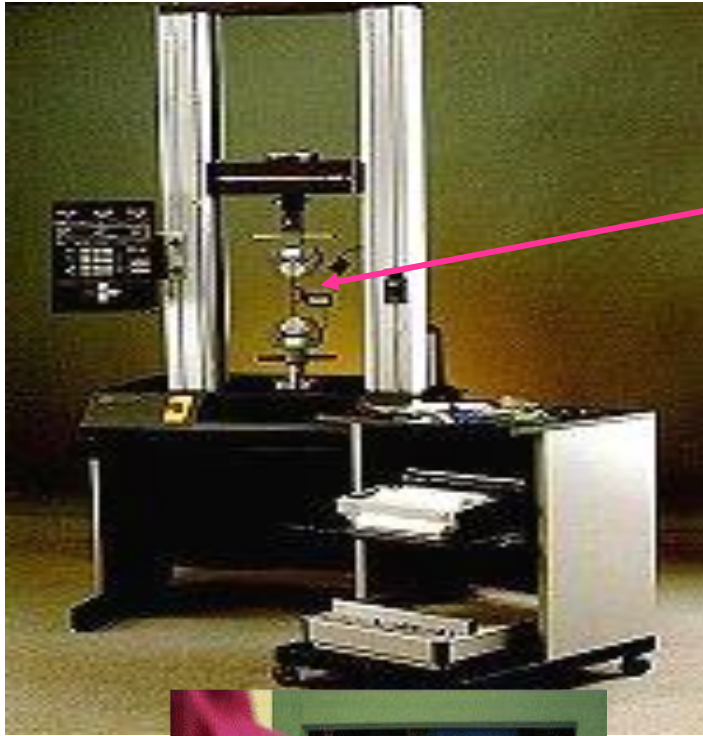
gauge length = portion of sample that will be evaluated ( $L_0$ )

- Other types of tests:
  - Compression: brittle materials (e.g., concrete)
  - Torsion: cylindrical tubes, shafts, etc.

- Geometry of a typical tensile test machine



# Universal Tensile Machine (UTM)



SAE1090 Hot rolled steel

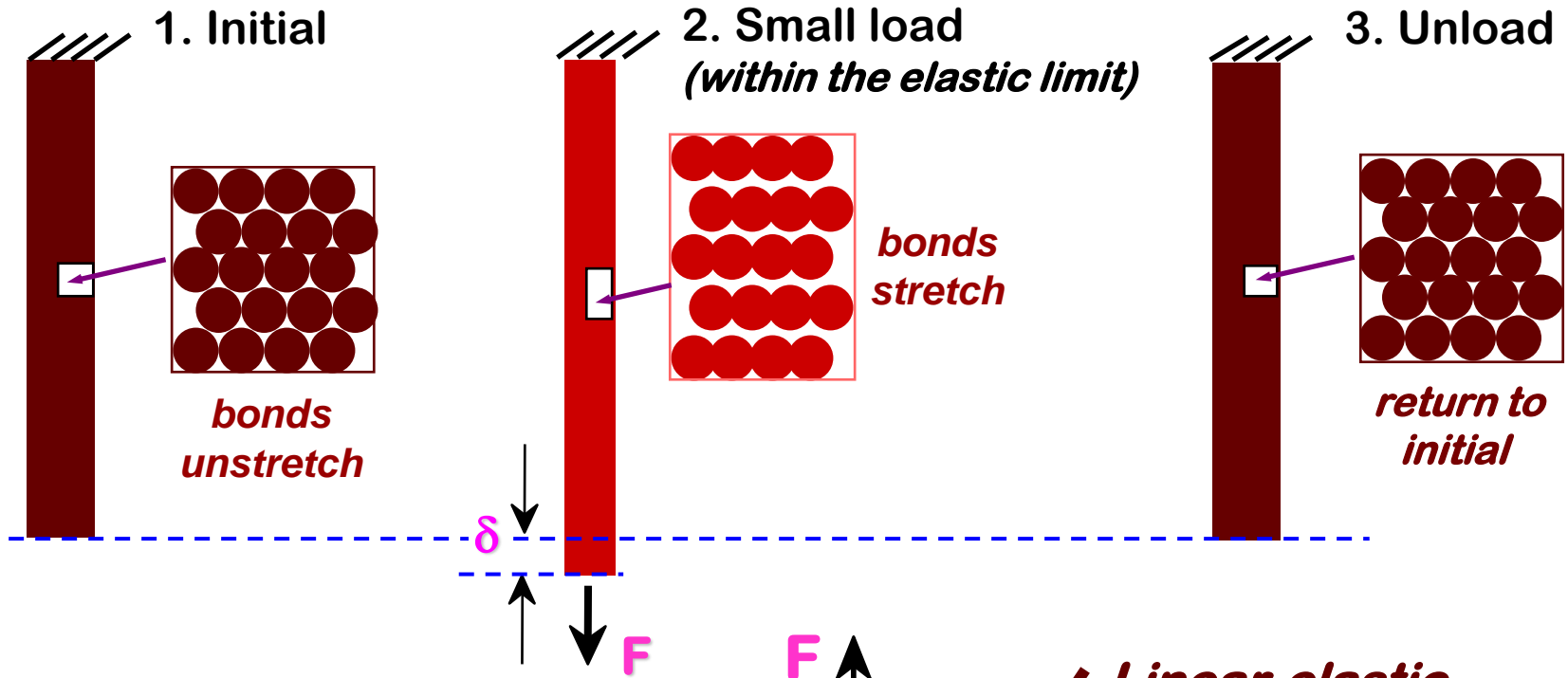


SAE1095 Spheroidized steel

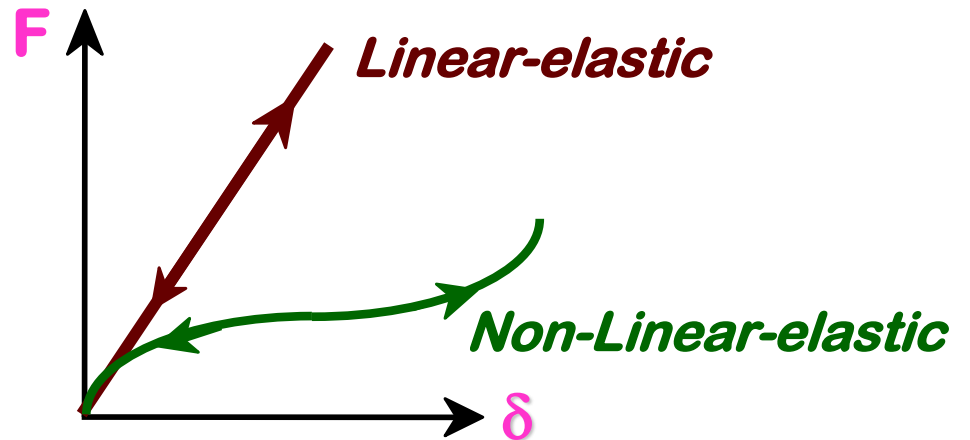


SAE1045 Hot rolled steel

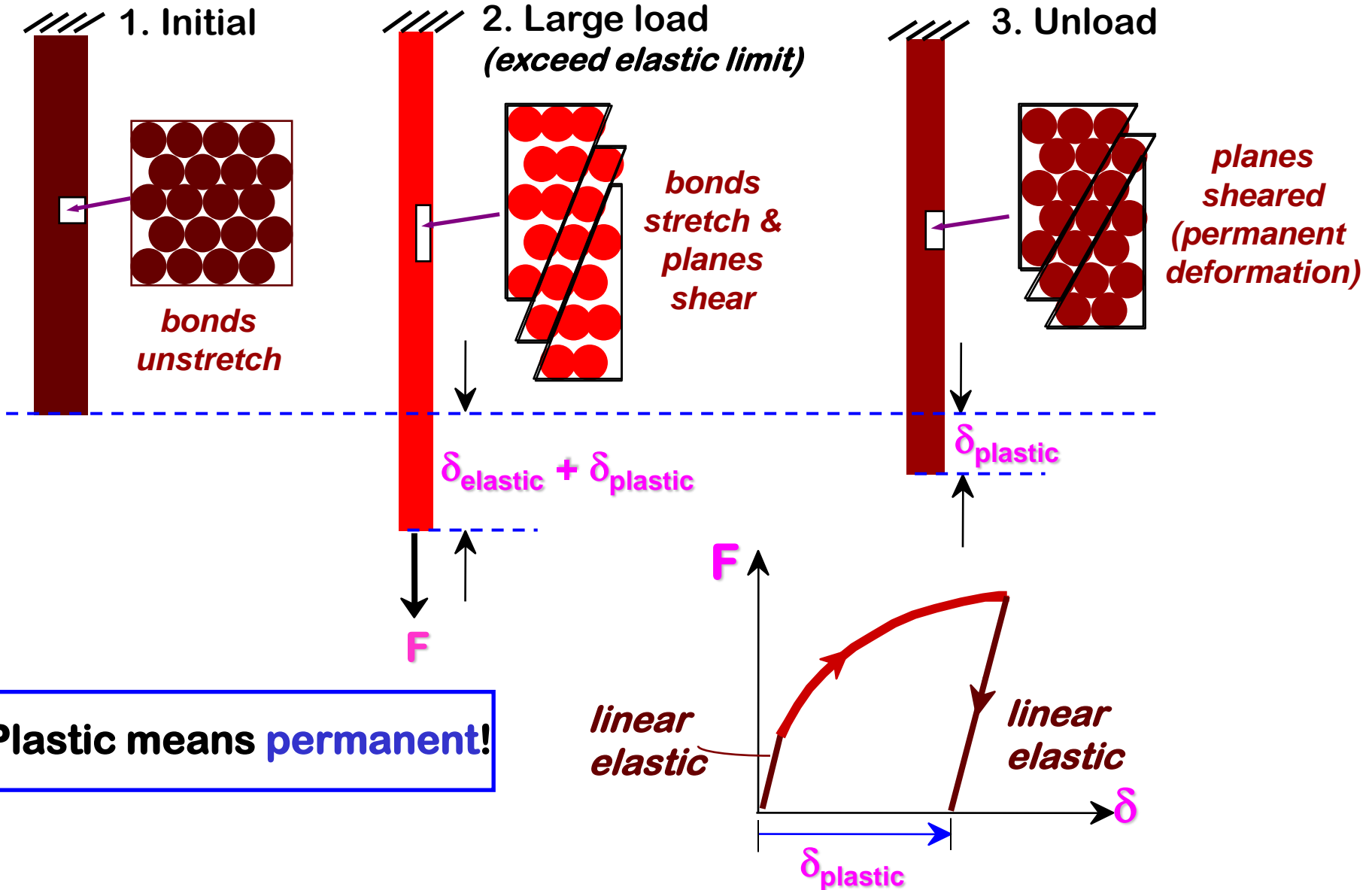
# Elastic Deformation



Elastic means **reversible!**

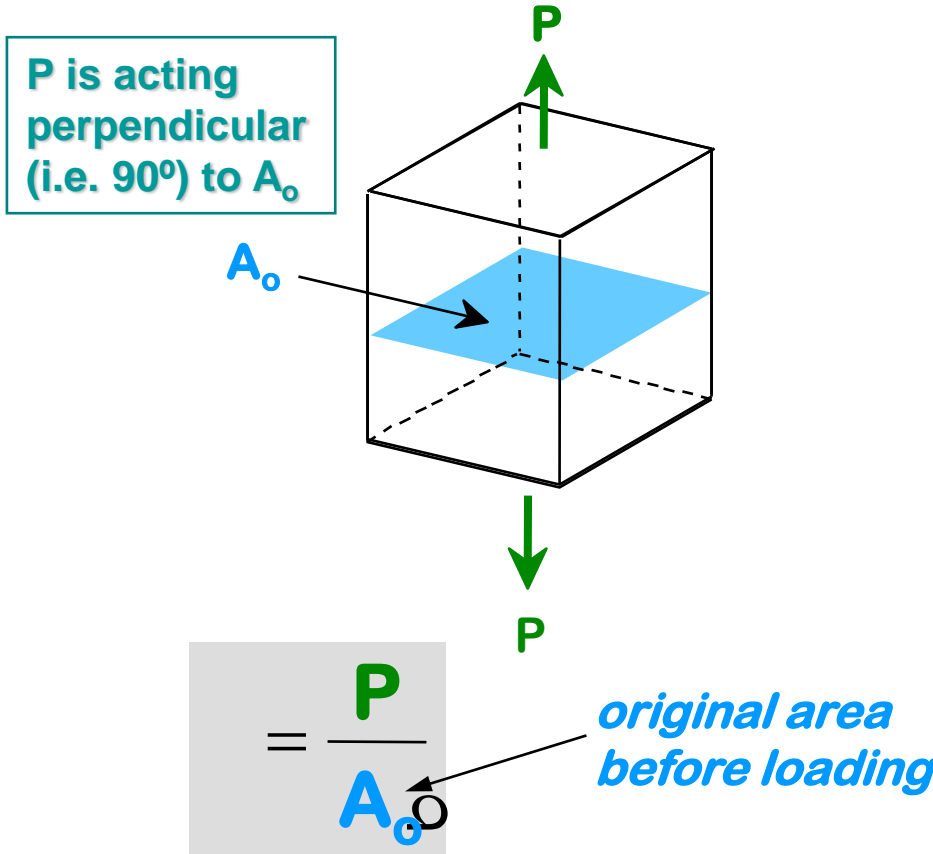


# Plastic Deformation

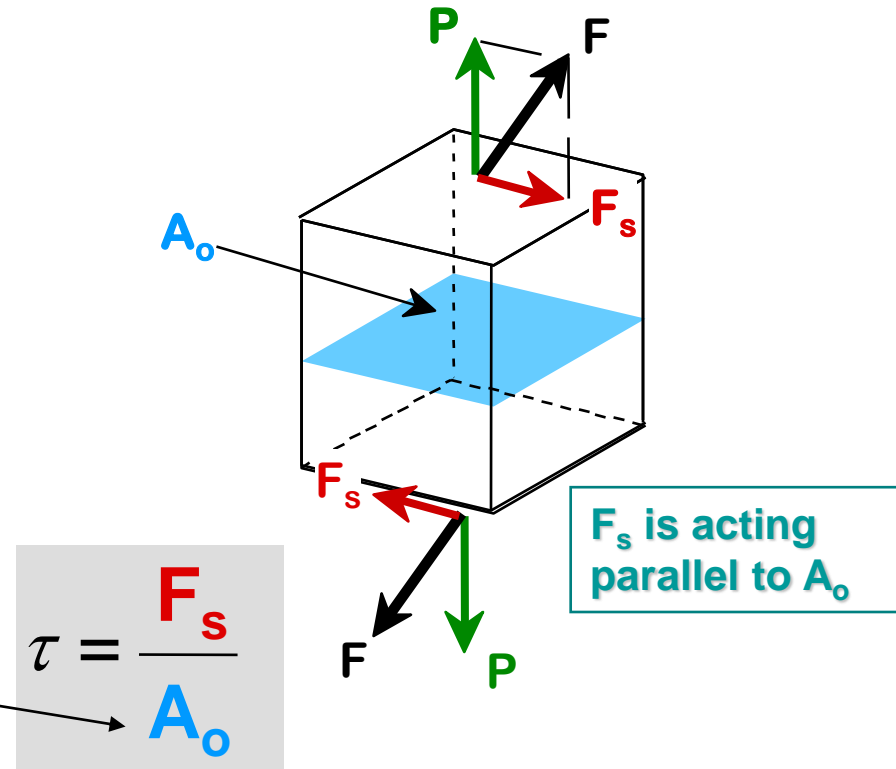


# Nominal (or Engineering) Stress

- **Tensile stress,  $\sigma$ :**



- **Shear stress,  $\tau$ :**



Stress has units of  $\text{N/m}^2$  or Pa

Note:

$1 \text{ N/m}^2 = 1 \text{ Pascal (Pa)}$

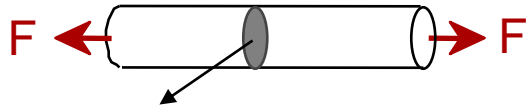
$1 \text{ N/mm}^2 = 1 \text{ MPa}$

*Stress and strain (rather than force and extension) are generally used when describing the deformation of solids because it is necessary to take into account the geometry and size of the sample.*



# Common States of Stress

- **Simple tension: Cable**



$A_o$  = original CSA  
(when unloaded)

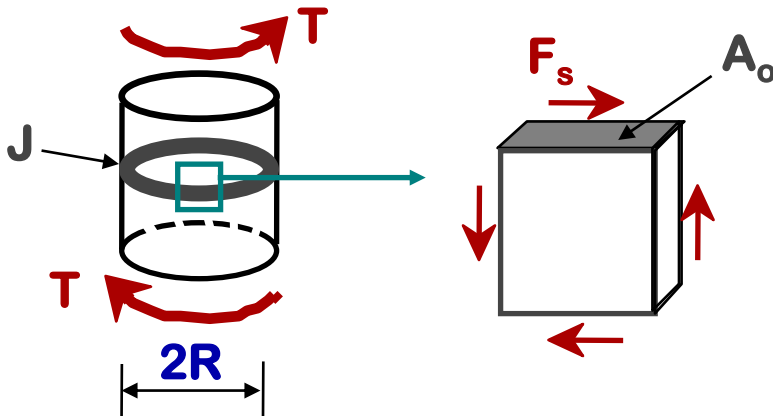
$$\sigma = \frac{F}{A_o}$$



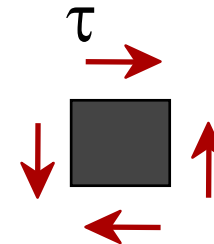
Tensile stress = +ve



- **Simple shear: Drive shaft**



$$\tau = \frac{F_s}{A_o}$$



Note:  $\tau = T.R/J$

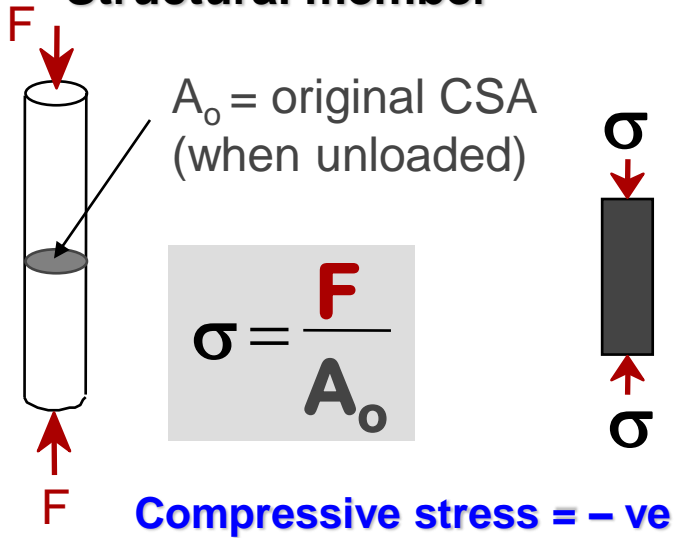
where T = torque

R = radius of shaft

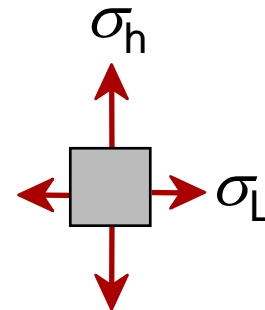
J = polar second moment of area

# Other Common States of Stress

- **Simple compression: Structural member**

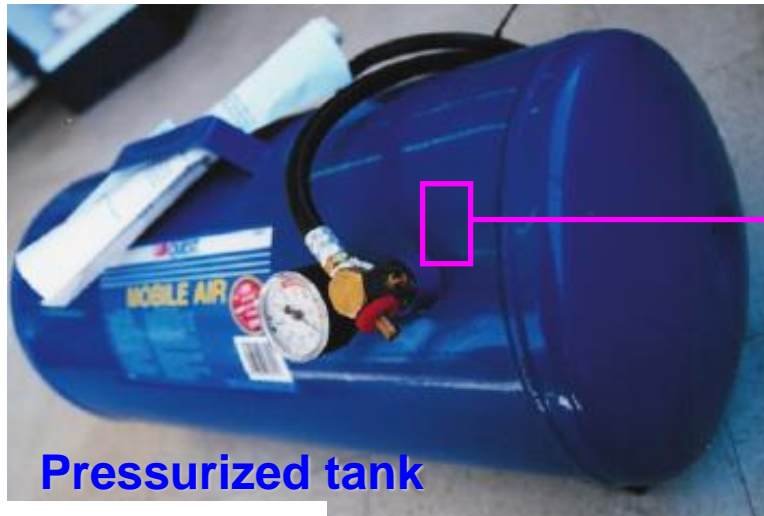


- **Bi-axial tension: Pressure vessel**



where  $\sigma_h$  = hoop or circumferential stress

$\sigma_L$  = longitudinal stress



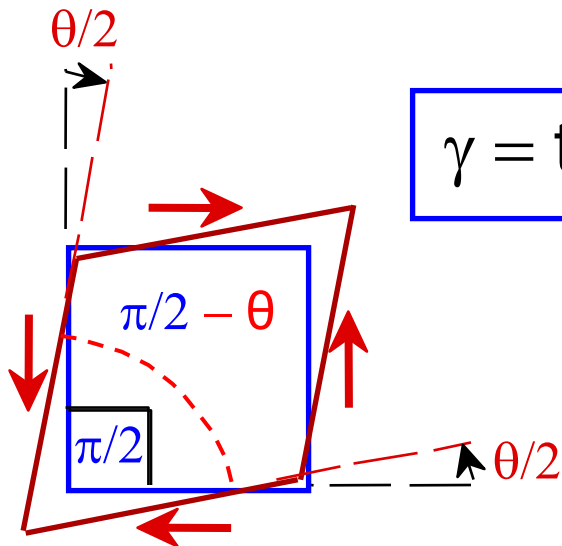
# Nominal (or Engineering) Strain

- **Tensile strain or Linear strain:**

$$\epsilon = \frac{\delta}{L_o}$$

+ve strain coz' tensile nature

- **Shear strain:**

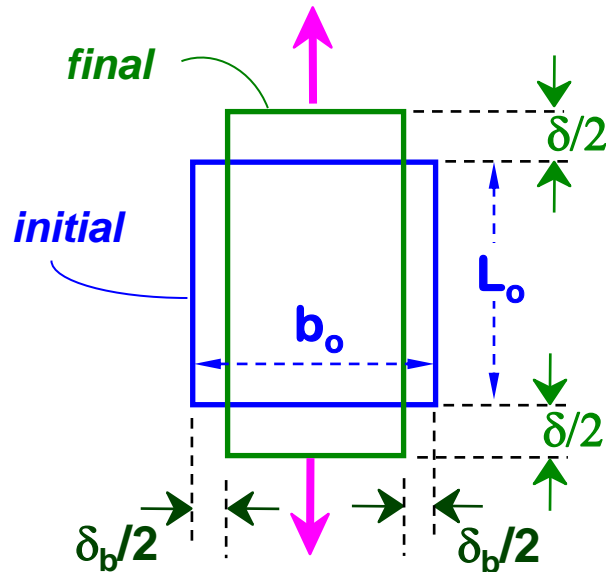


$$\gamma = \tan \theta$$

Where  $\theta$  = angle of shear in **radians**

Strain is always **DIMENSIONLESS** & often expressed in terms of percentage

e.g.  $\epsilon = 0.03$  or 3%



- **Lateral strain:**

$$\epsilon_b = \frac{-\delta_b}{b_o}$$

-ve strain coz' compressive nature

# Elastic Properties

- **Hooke's Law:** When the material is **stressed within the elastic limit**; the stress varies in proportional to the applied strain and can be related through:

$$\sigma = E \varepsilon$$

Where:

**E** is the matrix stiffness known as the **modulus of elasticity** or Young's modulus ;  $\varepsilon$  is the linear strain

$$\text{since } \sigma = \frac{F}{A_0} \quad \& \quad \varepsilon = \frac{\delta}{L_0} \quad ; \quad \therefore \frac{F}{A_0} = E \cdot \frac{\delta}{L_0} \quad \rightarrow \quad \delta = \frac{FL_0}{A_0 E}$$

- **Elastic Shear Modulus, G:**

$$\tau = G \gamma$$

**Units:**

**E = N/m<sup>2</sup> or GPa**

**G = N/m<sup>2</sup> or GPa**

# Elastic Properties: Poisson's Ratio

- Consider a material **loaded within the elastic limit**, say in the x-direction as shown:
- When we stretch the material in the x-direction, what happens in the radial (y- and z-) directions?  
*elongates in the x-dir. but gets thinner (compressed) in the y- and z-directions!*
- So we have axial or linear strain in the x-dir. which is taken as **positive strain (i.e. tensile nature)** and we have lateral strain in the lateral direction which is taken as **negative strain because compression!**
- Thus, the ratio between the two strains give **Poisson's Ratio ( $\mu$ )**:

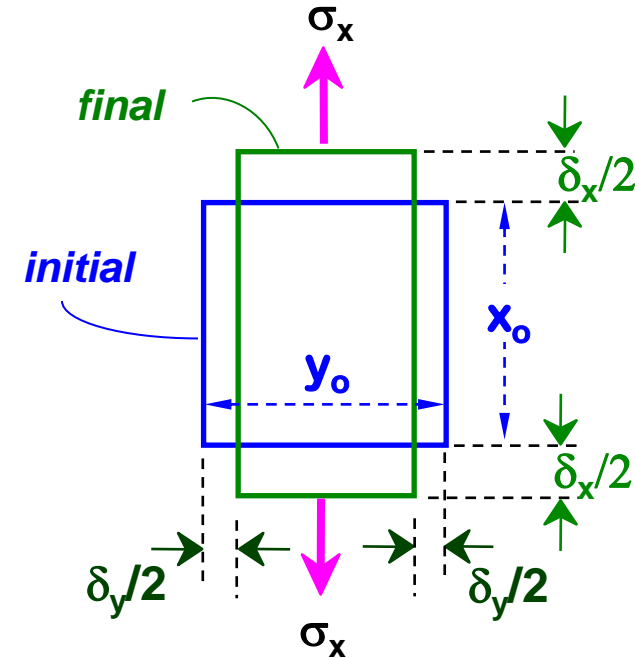
$$\mu = -\frac{\text{lateral strain}}{\text{linear strain}} = -\frac{\varepsilon_y}{\varepsilon_x} = -\frac{\varepsilon_z}{\varepsilon_x}$$

$$\text{where } \varepsilon_x = \frac{\delta_x}{x_0}$$

$$\& \varepsilon_y = \frac{-\delta_y}{y_0}$$

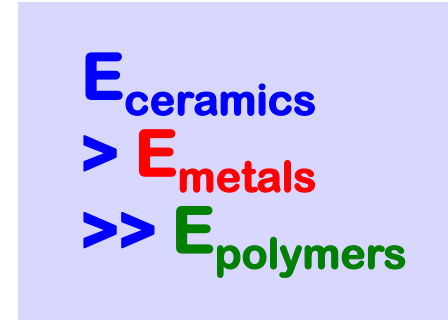
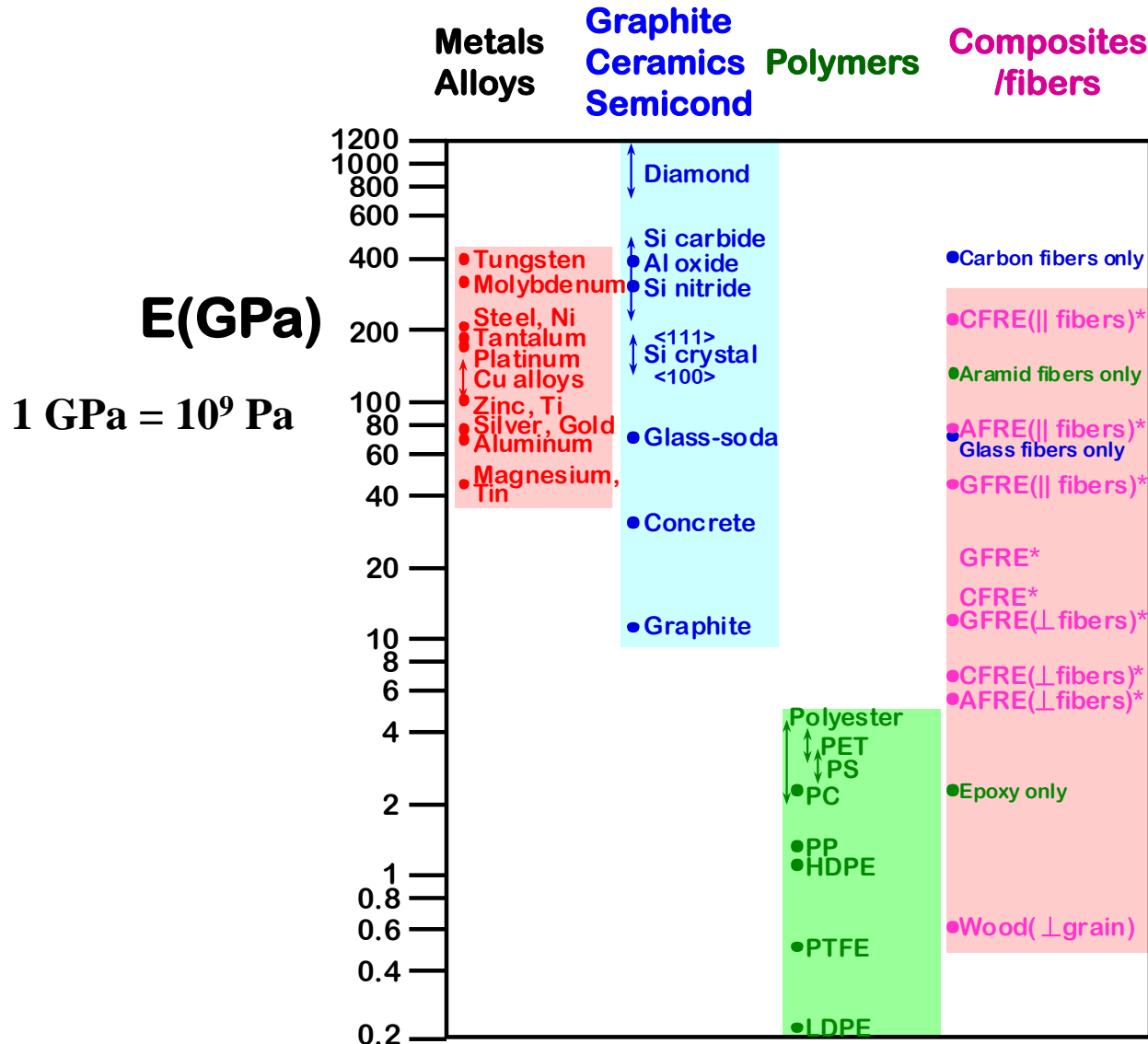
- For Isotropic material:  **$E = 2G(1 + \mu)$** ;  
For most metals  **$G \sim 0.4E$**

- However, many materials, especially crystals, are **NOT Isotropic**; so their properties depend on crystals orientation



**$\mu$  = dimension less, positive & is less than 1**  
 e.g. metals:  $\mu \sim 0.33$   
 ceramics:  $\mu \sim 0.25$   
 polymers:  $\mu \sim 0.40$

# Young's Moduli: Comparison



Based on data in Table B2, *Callister 6e*.  
 Composite data based on reinforced epoxy with 60 vol% of aligned carbon (CFRE), aramid (AFRE), or glass (GFRE) fibers.

# Stiffness and Modulus

- **Stiffness** is a measure of an **object's** resistance to elastic deformation or strain
  - depends on material type
  - depends on thickness and shape of object

$$E \propto \left( \frac{dF}{dr} \right)_{r_0}$$

- **Modulus** is a measure of a **material's** resistance to elastic deformation or strain
- or modulus is a measure of resistance to separation of adjacent atoms, i.e., inter-atomic bonding forces
  - independent on shape

↑ **E** ∝ **Stiffness** ↑ ∝ **Elastic strain** ↓

# Definition of True Stress and True Strain

- True stress and True strain are calculated based on **incremental change in sample geometry**.

- Consider the case of axial loading:

- True Stress:

$$\sigma_t = \frac{F}{A_t}$$

- True Strain:

$$d\varepsilon = \frac{d\delta}{L} \quad \text{.....for limits between } L_o \text{ and } L_f:$$

$$\varepsilon_t = \int_{L_o}^{L_f} \frac{d\delta}{L} = \log_e \left[ \frac{L_f}{L_o} \right] = \ln \left[ \frac{L_f}{L_o} \right] = \ln \left[ \frac{A_o}{A_f} \right]$$

Where

**F** = applied force

**A<sub>t</sub>** = instantaneous CSA or true area

**A<sub>o</sub>** = initial CSA

**L<sub>f</sub>** = final length

**L<sub>o</sub>** = initial length

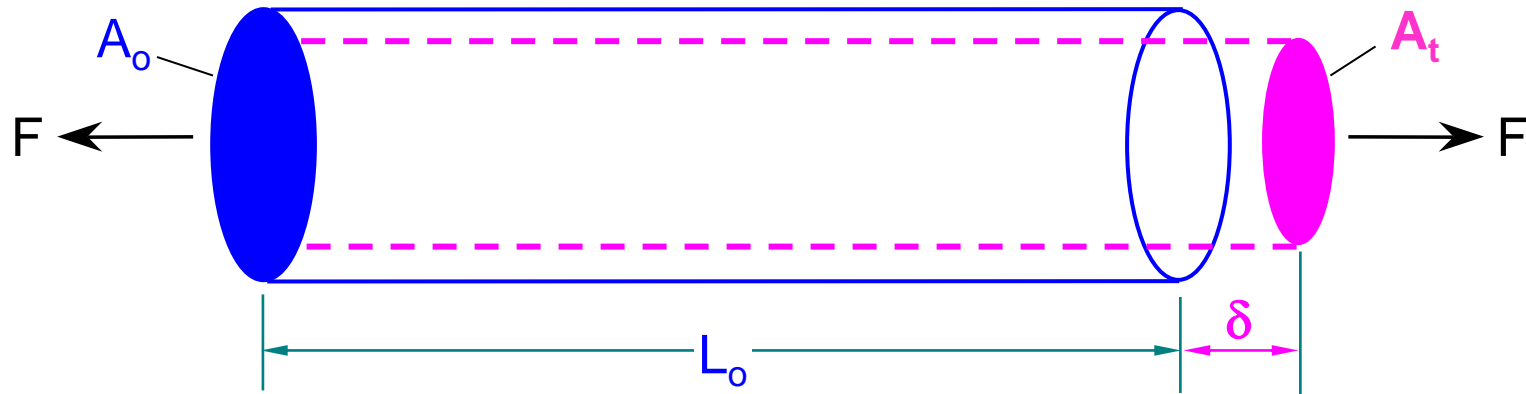
Since there is no lost of material during deformation,  
∴ vol. = constant !:

$$\left. \begin{array}{l} V_o = V_f \\ A_o L_o = A_f L_f \end{array} \right\} \therefore \frac{L_f}{L_o} = \frac{A_o}{A_f}$$

- For **small values of strain (within the elastic limit)**, engineering and true strains **are equivalent** – **but they rapidly diverge for LARGE Strains (i.e. when loaded above elastic limit)**
- True stresses and strains must be considered during manufacturing processes that involve **plastic deformation (PD)**.



# Nominal (or Engineering) Stress Vs. True Stress



- Consider the homogeneous bar shown above, subjected to an axial tensile force ( $F$ ).
- There are two ways to calculate stress:

– Based on the original area, **nominal or eng. stress**:

$$\sigma_n = \frac{F}{A_o}$$

– Based on the **instantaneous area, true stress**:

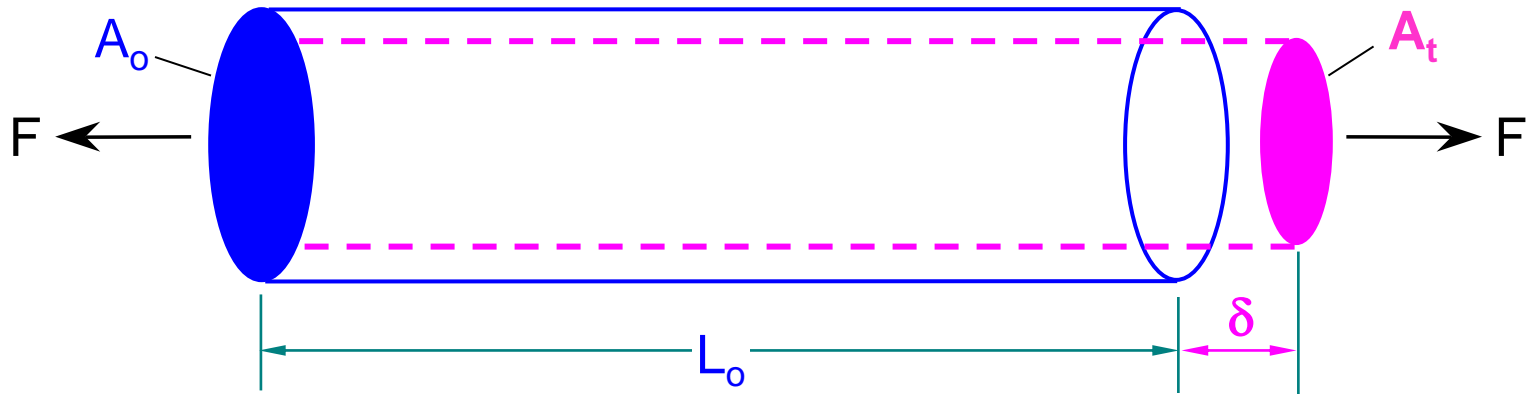
$$\sigma_t = \frac{F}{A_t}$$

**Where**

$A_o$  = initial cross sectional area (CSA);  $L_o$  = initial length;

$A_t$  = instantaneous CSA;  $\delta$  = change in length;

# Nominal (or Engineering) Strain Vs. True Strain



- Consider the homogeneous bar shown above, subjected to an axial tensile force ( $F$ ).
- There are two ways to calculate strain:

– Based on the original length, *nominal strain*:

$$\epsilon_n = \frac{\delta}{L_o} = \frac{L_f - L_o}{L_o}$$

– Based on the instantaneous length, *true strain*:

$$\epsilon_t = \ln\left(\frac{L_f}{L_o}\right) = \ln\left(\frac{A_o}{A_f}\right)$$

Where

$L_o$  = initial length;  $\delta$  = change in length;  $L_f$  = instantaneous or final length

# Relationship Between Nominal (or Eng.) & True Values

From previous slide:

$$\varepsilon_t = \ln \left( \frac{L_f}{L_o} \right) \text{--- (1)}$$

$$\varepsilon_n = \frac{L_f - L_o}{L_o} \text{ or } L_f = L_o + \varepsilon_n L_o \text{--- (2)}$$

Put (2) into (1):  $\varepsilon_t = \ln \left( \frac{L_o + \varepsilon_n L_o}{L_o} \right)$  ;  $\therefore \varepsilon_t = \ln (1 + \varepsilon_n) \text{--- (3)}$

During deformation, note that: **Initial vol. of sample = instantaneous vol. of sample**  
(since mass & density remain the same)

$$\text{i.e. } V_o = V_t \text{ ; } A_o L_o = A_t L_f \text{ (substitute for } L_f \text{ from Eq. 2)}$$

$$A_o L_o = A_t (L_o + \varepsilon_n L_o)$$

$$\therefore A_o = A_t (1 + \varepsilon_n) \text{--- (4)}$$

Also, at any instance during the loading:

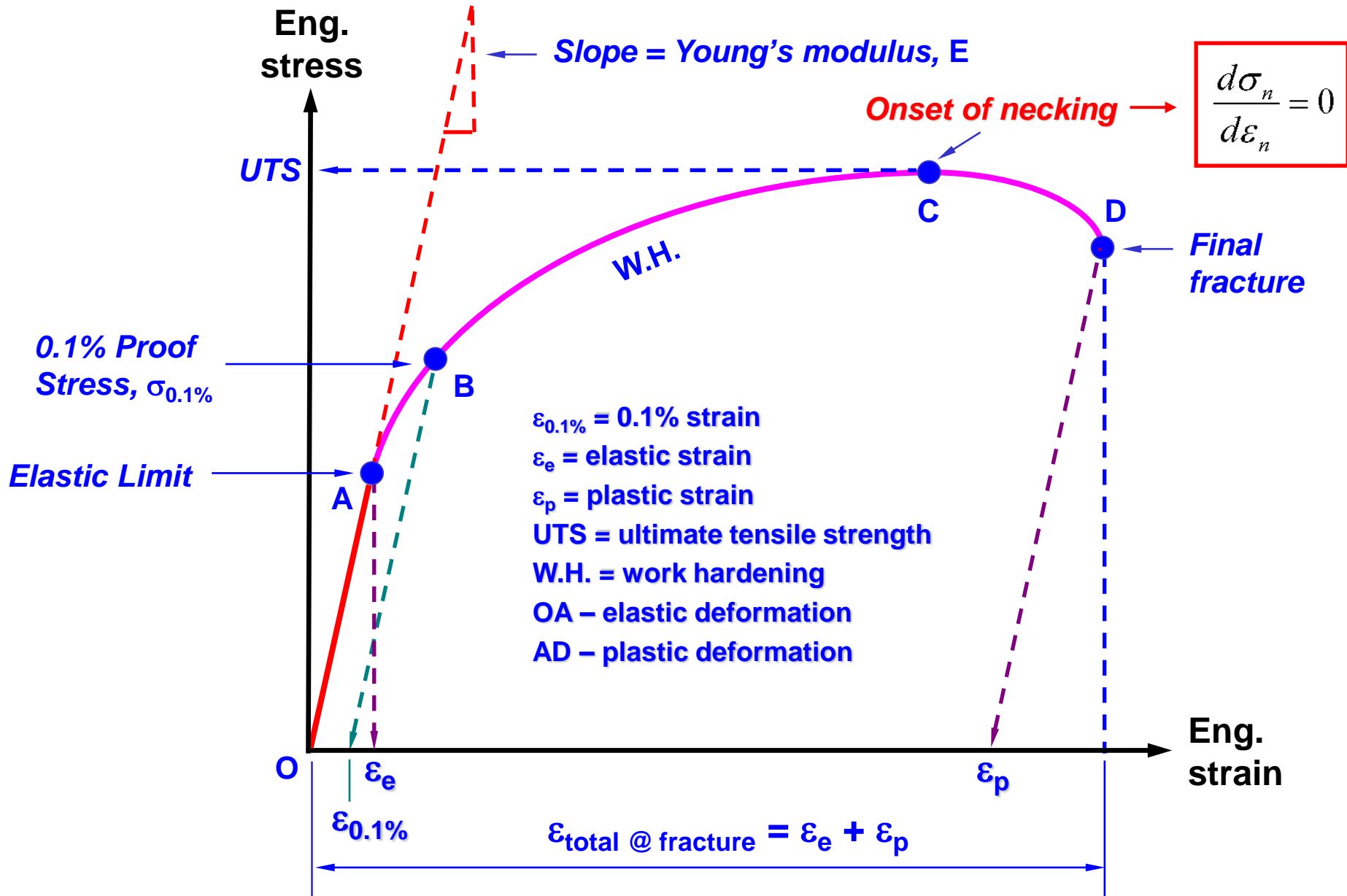
$$F_n = F_t$$

$$\sigma_n A_o = \sigma_t A_t \text{ (substitute for } A_o \text{ from Eq. 4)}$$

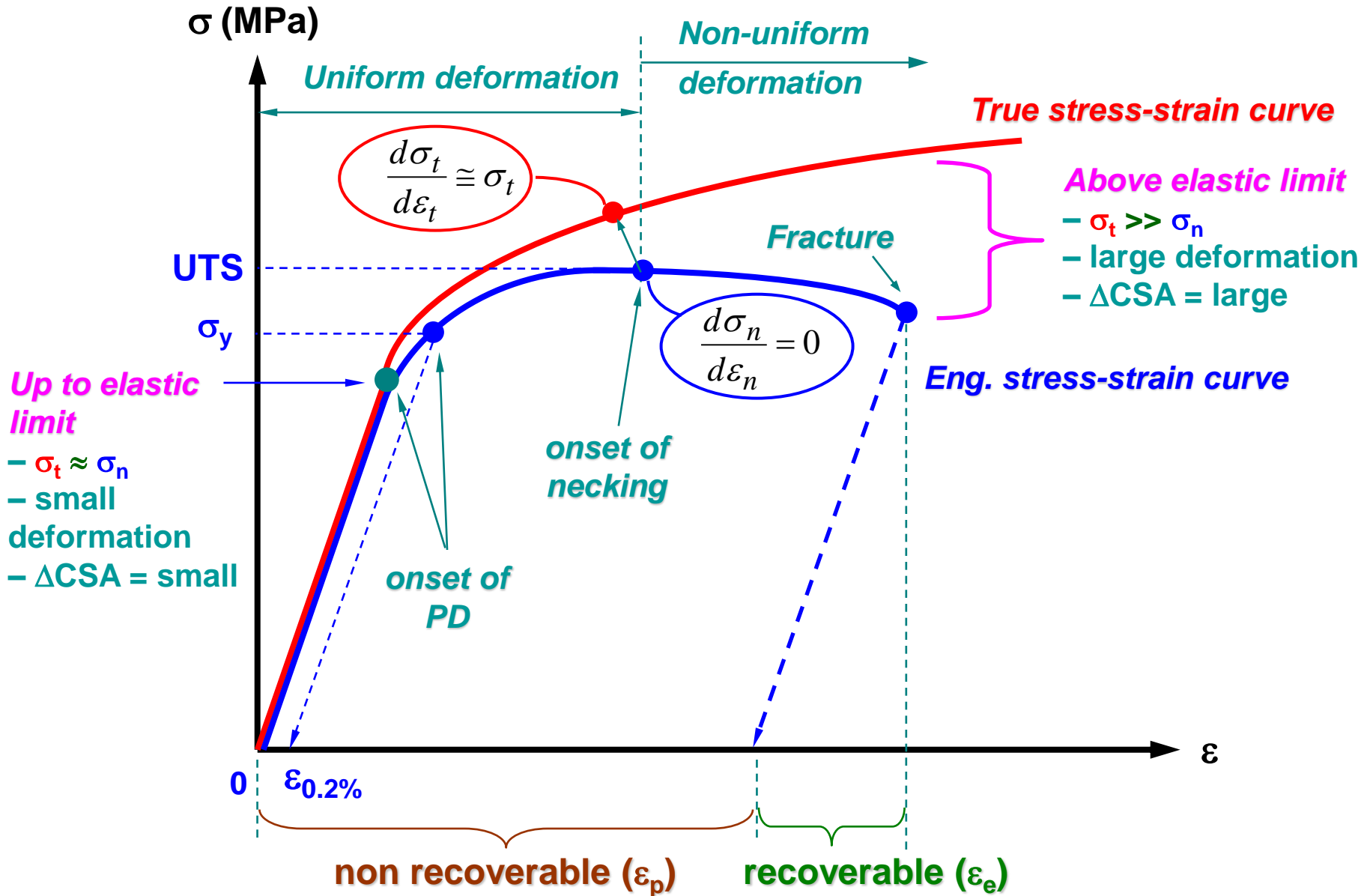
$$\sigma_n A_t (1 + \varepsilon_n) = \sigma_t A_t \text{ ; } \therefore \sigma_t = \sigma_n (1 + \varepsilon_n) \text{--- (5)}$$

**$\sigma_t \cong \sigma_n$  for high E and small  $\varepsilon$  but not true for materials undergo large  $\varepsilon$ , e.g., rubber where CSA may change significant**

# Engineering (or Nominal) Stress–Strain Curve



# True Stress–Strain Curve: Comparison



# Plastic (Permanent) Deformation (PD)

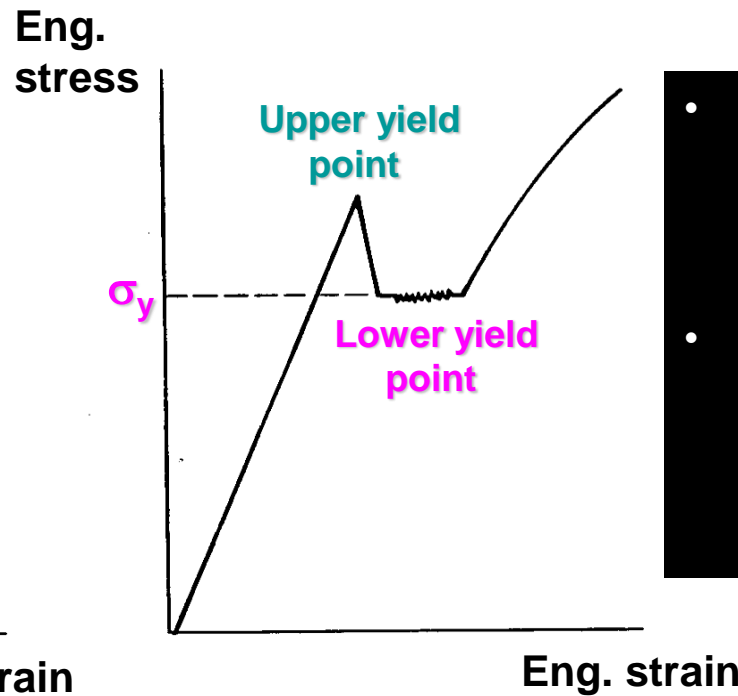
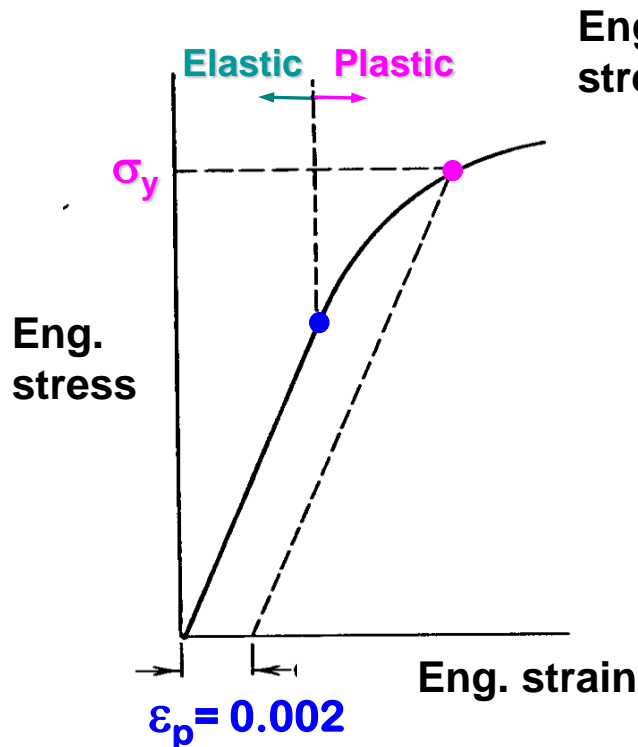
- **1**-PD is permanent and non-recoverable
- **2**-PD **occurs** when the applied load **exceed** the **elastic limit**
- **3**-From this point onwards, the material **DO NOT** obeys the Hooke's law and stress is **no longer** proportional to the strain
- **4** -PD normally occurs at lower temperatures, i.e.  $T < T_{\text{melt}}/3$
- **5**-PD corresponds to **breaking of bonds** with original atom neighbors and **reforming bonds** with new neighbors; **∴ atoms or molecules move relative to one another**
- **6**-Transition from elastic to plastic is **gradual for** most metals
- **7**-For crystalline solids, deformation process is by means of slip which involves dislocation motion.
- **8**-Yielding = stress level at which PD begins
- **∴ 9**- The yield stress,  $\sigma_y \rightarrow$  is a measure of material's resistance to PD

# Yield Strength or Stress ( $\sigma_y$ )

- $\sigma_y$  is the stress at which *noticeable* plastic deformation has occurred; For most metals yielding occurs when the plastic strain is,  $\epsilon_p = 0.002$  or 0.2%

e.g. Grey cast iron

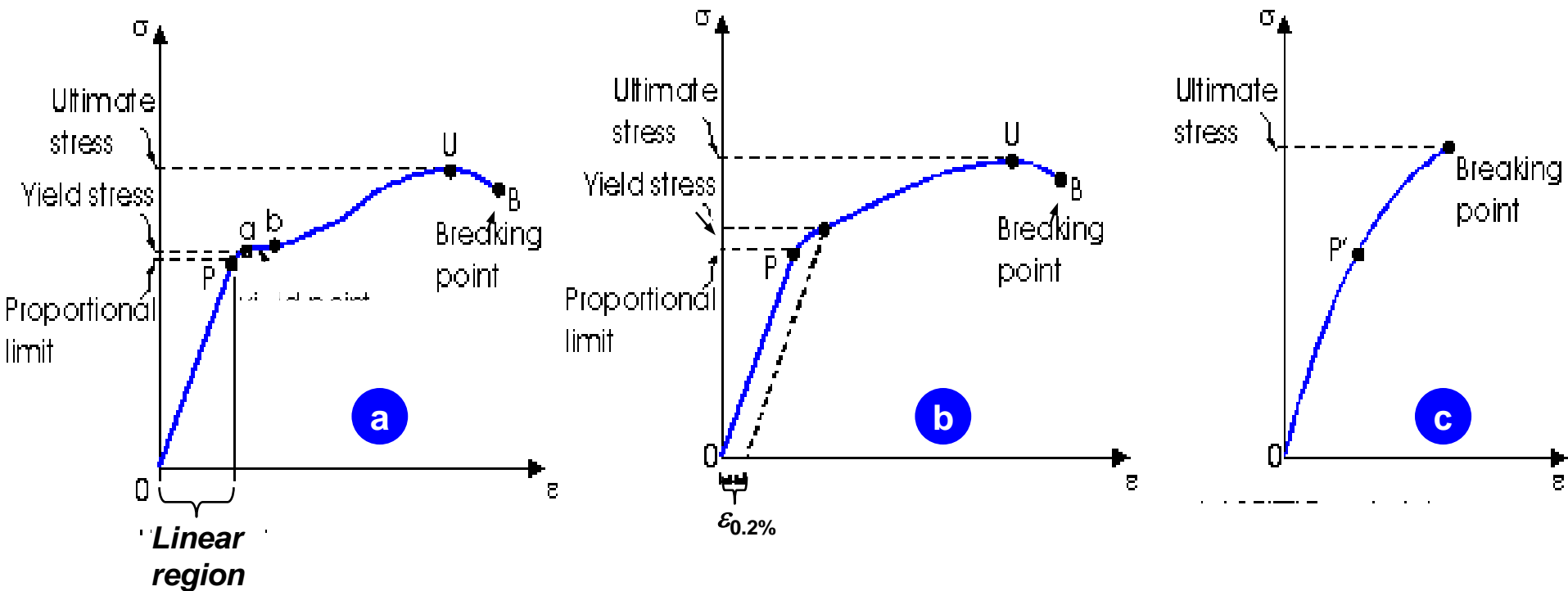
e.g. Low carbon steels



- Point of yielding** = initial departure from linearity of Eng. Stress Vs. Eng. Strain curve
- In design, eng. components must not deform plastically. Thus,  **$\sigma_y$  is taken as design criteria !!**

- Sometimes, it is difficult to determine exactly the position of the yield point (as shown above for grey cast iron); It is common to take the yield stress as the 0.2% proof stress, i.e. the stress corresponds to **0.002 strain offset** as shown above.

# Yield Strength of Materials

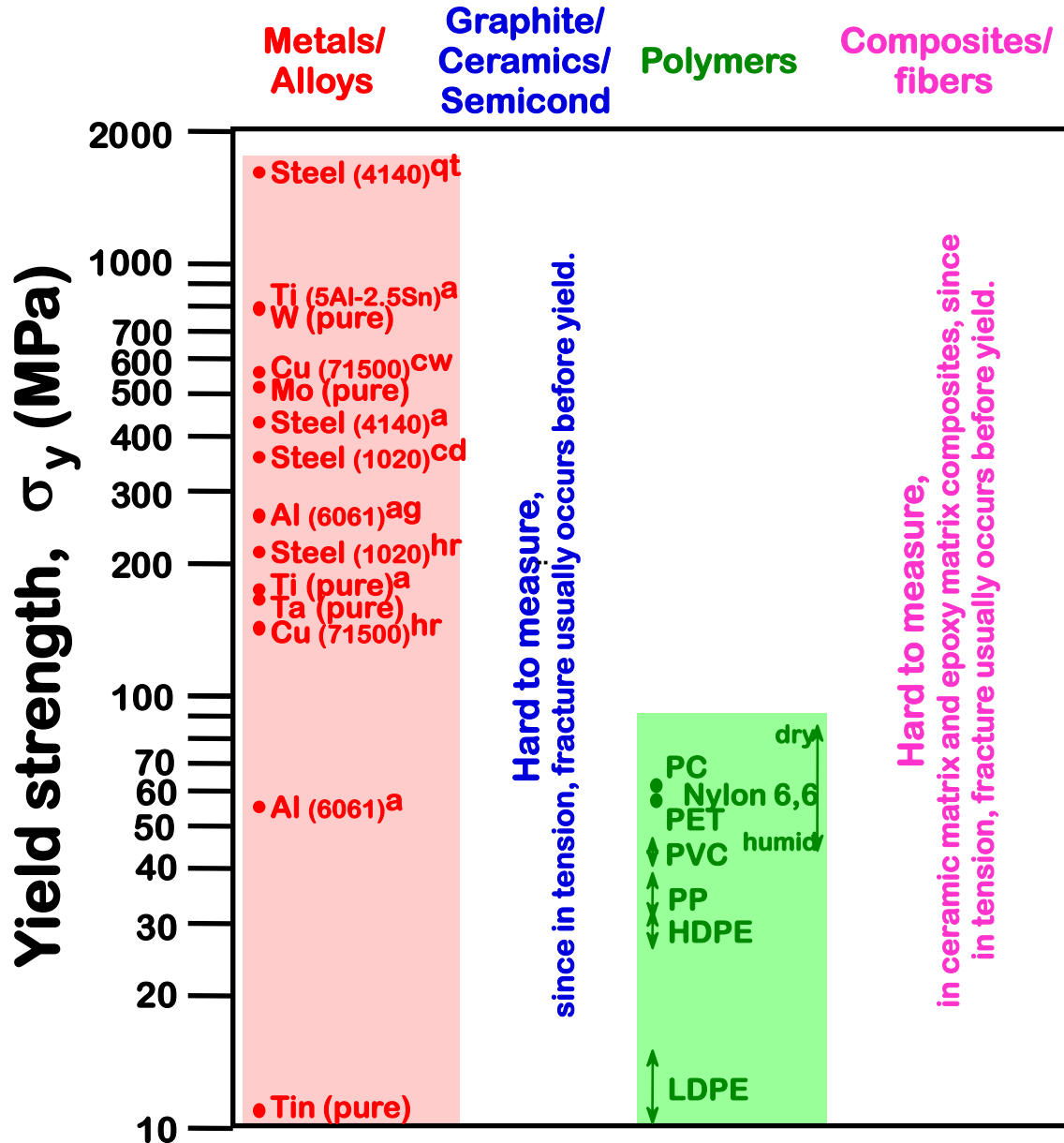


The stress-strain curves for three different types of material:

- (a) Low-carbon steel, a ductile material with a distinct yield point.
- (b) A ductile material, such as Al alloy  $\rightarrow$  no define yield point  $\rightarrow$  take  $\sigma_y$  @ 0.2% strain ( $\epsilon_{0.2\%}$ )
- (c) A brittle material, e.g. glass, ceramics, cast iron, in compression  $\rightarrow$  take  $\sigma_y = \sigma_{\text{fracture}}$



# Yield Strength: Comparison



$$\sigma_y(\text{ceramics}) > \sigma_y(\text{metals}) >> \sigma_y(\text{polymers})$$

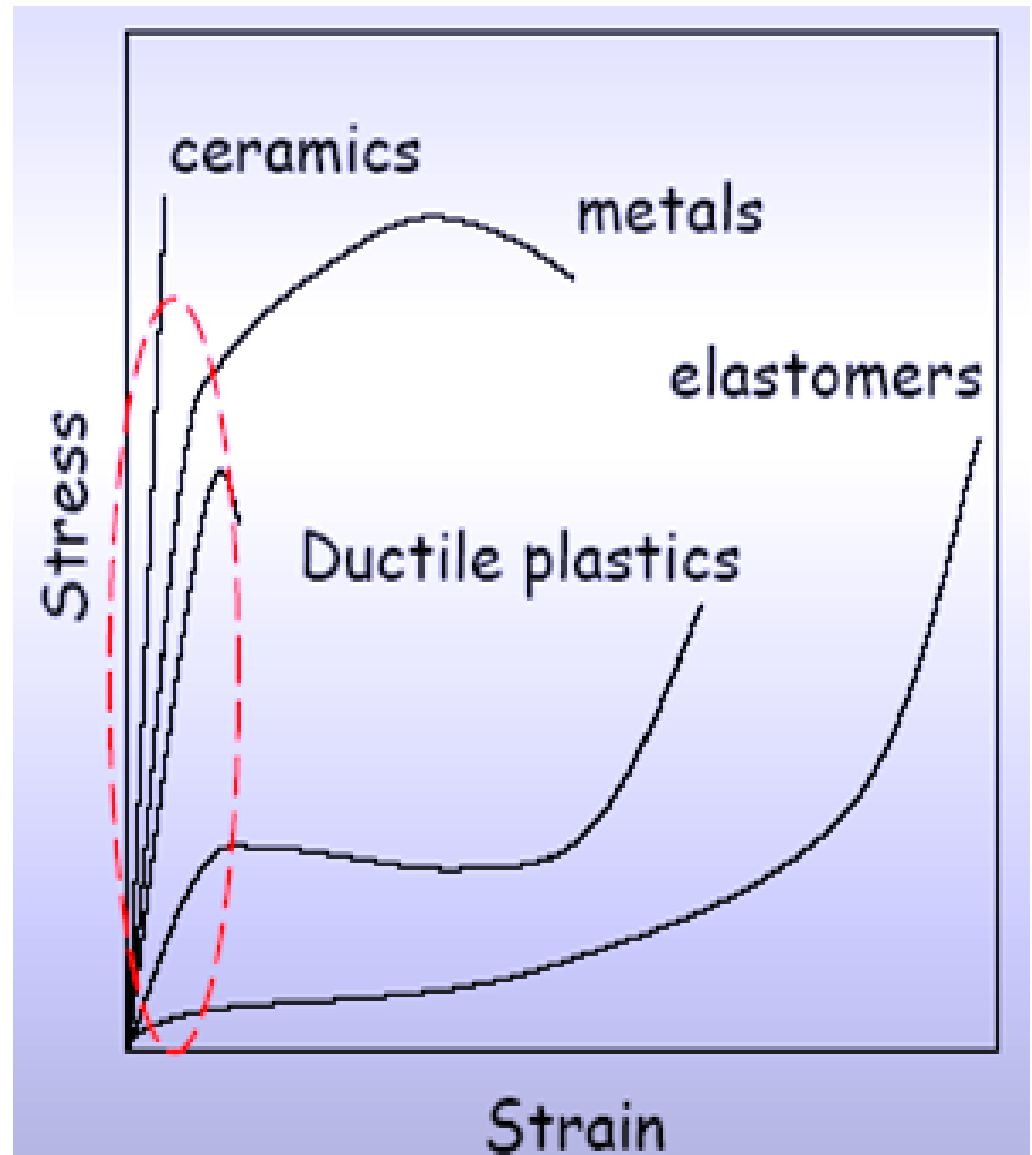
Room T values

Based on data in Table B4, *Callister 6e*.

- a = annealed
- hr = hot rolled
- ag = aged
- cd = cold drawn
- cw = cold worked
- qt = quenched & tempered

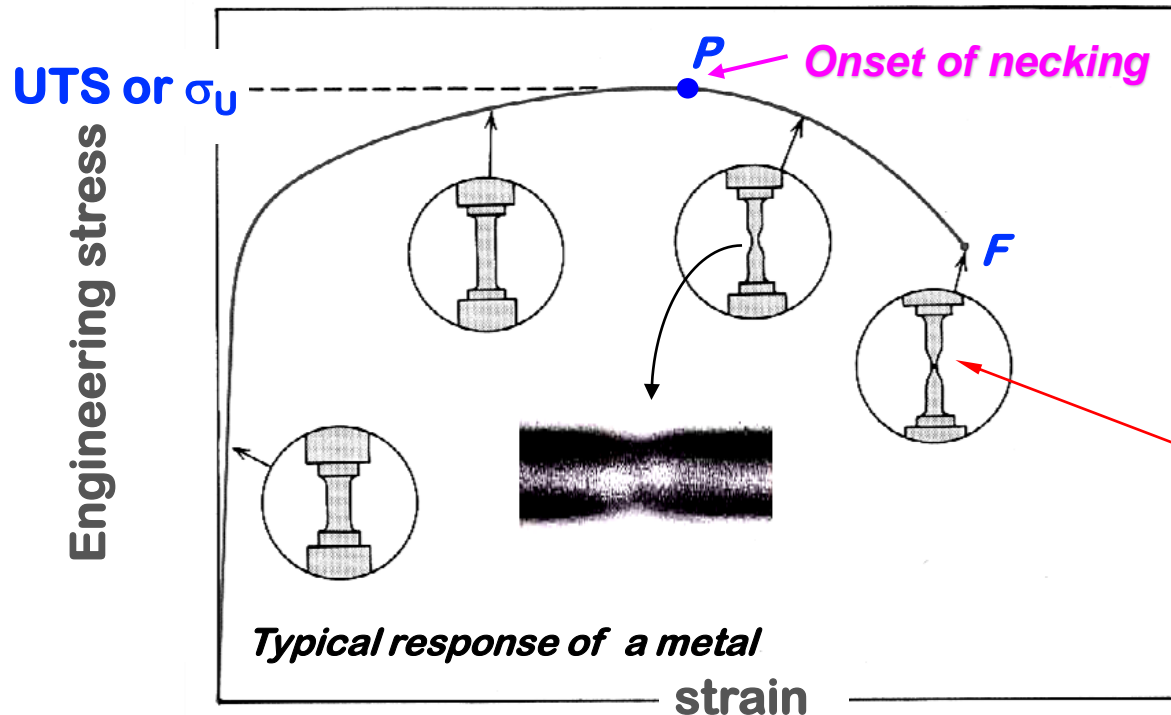
# Yield Strength: Design Criteria

- Schematic comparison of tensile behavior of common engineering materials.
- Design criteria *vary with material classes*.
- A general rule of thumb:
  - For metals:  $\sigma_y = \sigma_{0.2\%}$
  - For ceramics & brittle plastics:  $\sigma_y = \sigma_{\text{fracture}}$
  - For ductile plastics:  $\sigma_y = \sigma_{1\%}$
  - For composites:  $\sigma_y = \sigma_{0.5\%}$

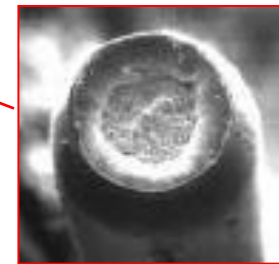


# Tensile Strength (Ultimate Tensile Strength, UTS)

- UTS or  $\sigma_U$  is the **maximum possible** engineering stress in tension.



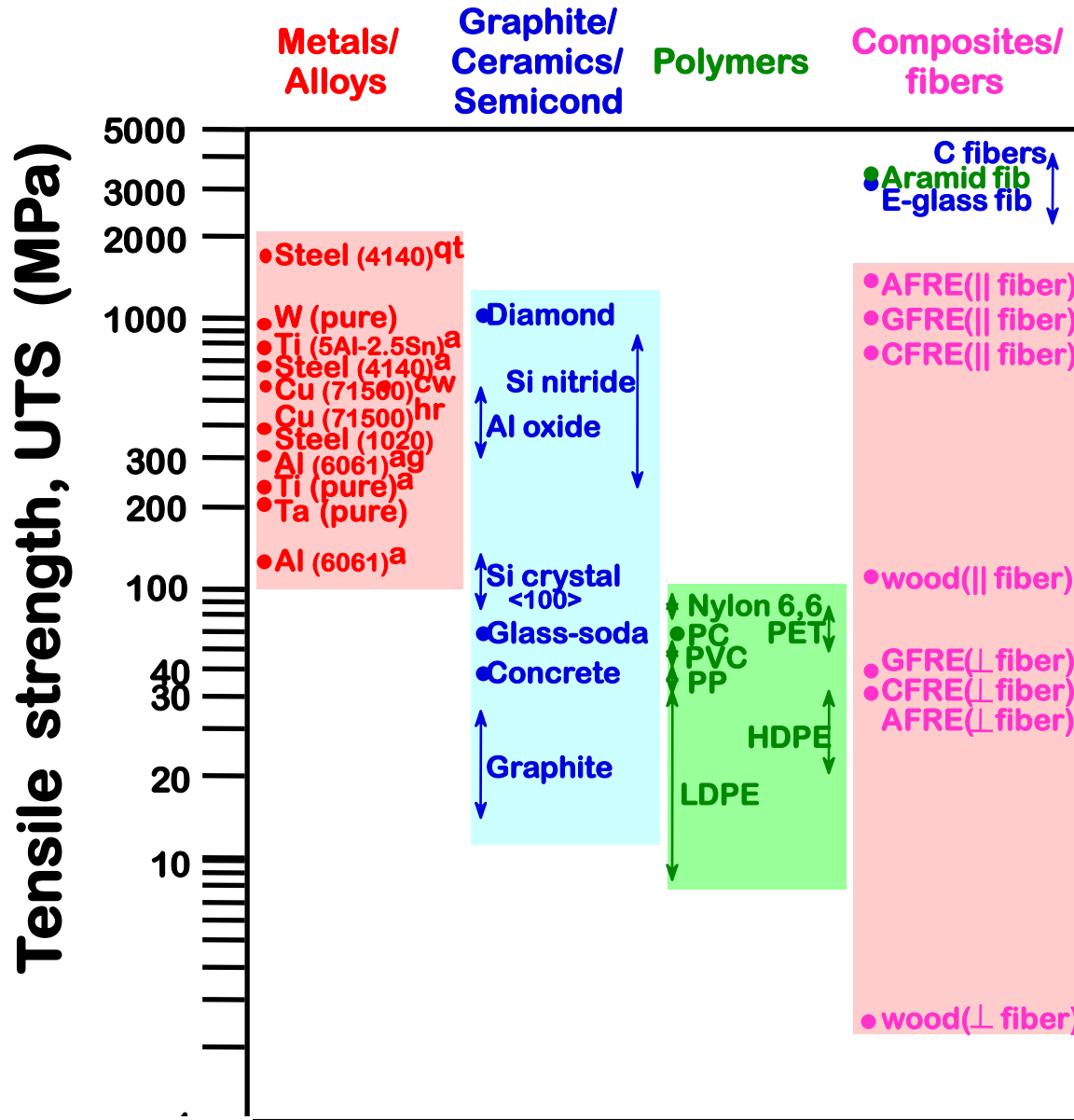
- **Uniform** deformation up to  $P$
- Beyond point  $P$ , **necking** resulted; i.e., deformation confined at this **constriction**.



Fracture strength =  
Stress at fracture

- **Metals:** occurs when noticeable **necking** starts.
- **Ceramics:** occurs when **crack propagation** starts.
- **Polymers:** occurs when **polymer backbones** are aligned and about to break.
- **For design, use  $\sigma_y$  and not UTS** (due to large PD had occurred at UTS). *UTS is only use for deep drawing or other metal forming process.*

# Tensile Strength: Comparison



$UTS_{(ceramics)}$   
 $\sim UTS_{(metals)}$   
 $\sim UTS_{(composites)}$   
 $\gg UTS_{(polymers)}$

## Room T values

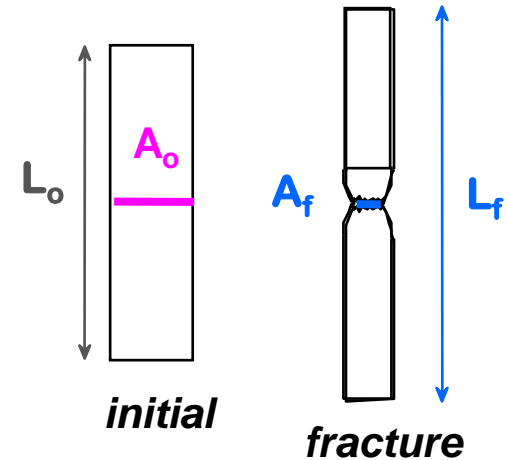
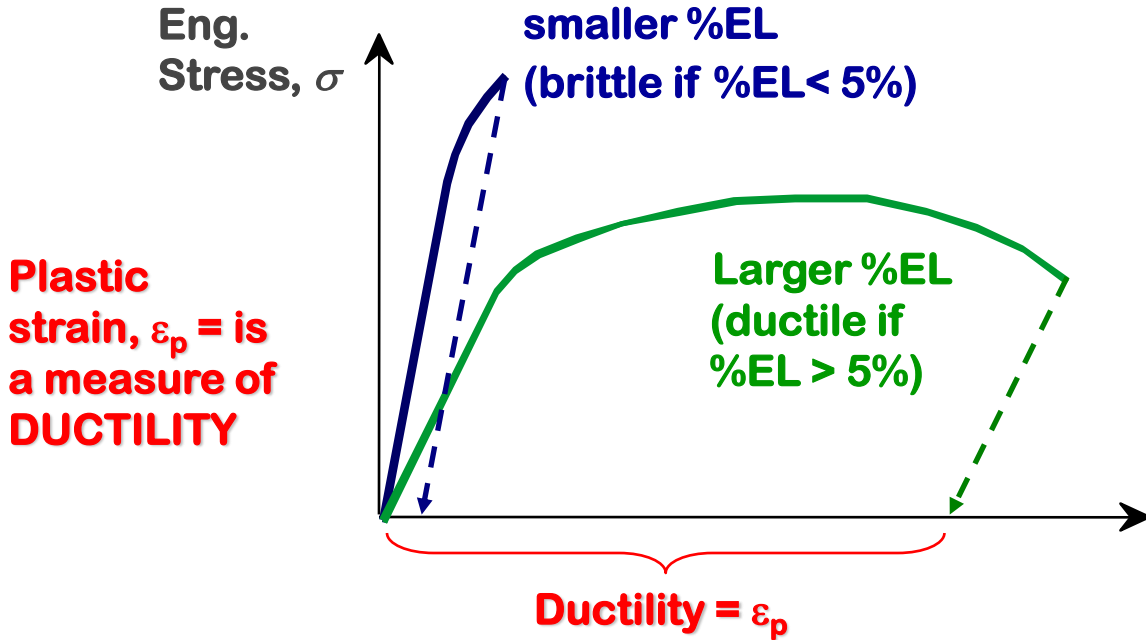
Based on data in Table B4, *Callister 6e*.

- a = annealed
- hr = hot rolled
- ag = aged
- cd = cold drawn
- cw = cold worked
- qt = quenched & tempered
- AFRE, GFRE, & CFRE = aramid, glass, & carbon fiber-reinforced epoxy composites, with 60 vol% fibers.

# Ductility

- Is define as **plastic tensile strain at fracture** and can be expressed in terms of %elongation (EL) or % reduction in area (AR):

$$\%EL = \frac{(L_f - L_o)}{L_o} \times 100$$

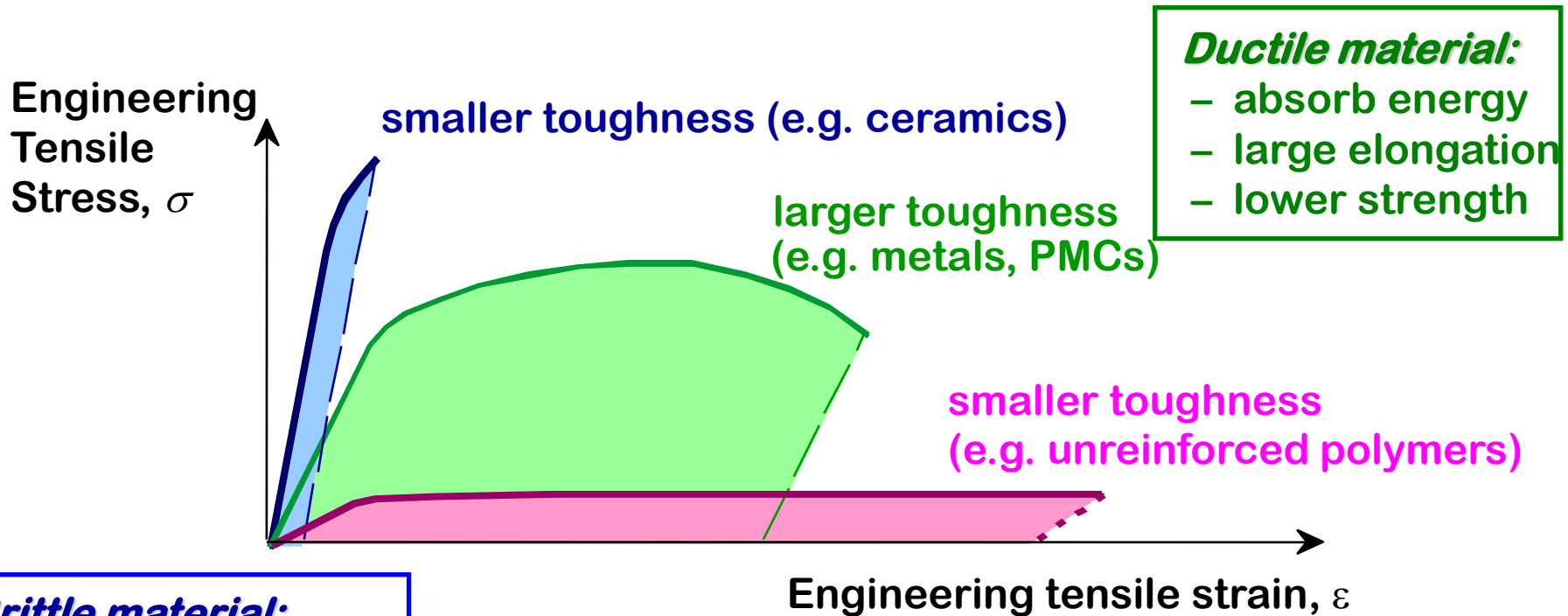


- % reduction in area (AR):
- Note that %AR and %EL are often comparable.
  - Reason: crystal slip does not change material volume.
  - However it is possible that %AR > %EL if internal voids form in neck region.

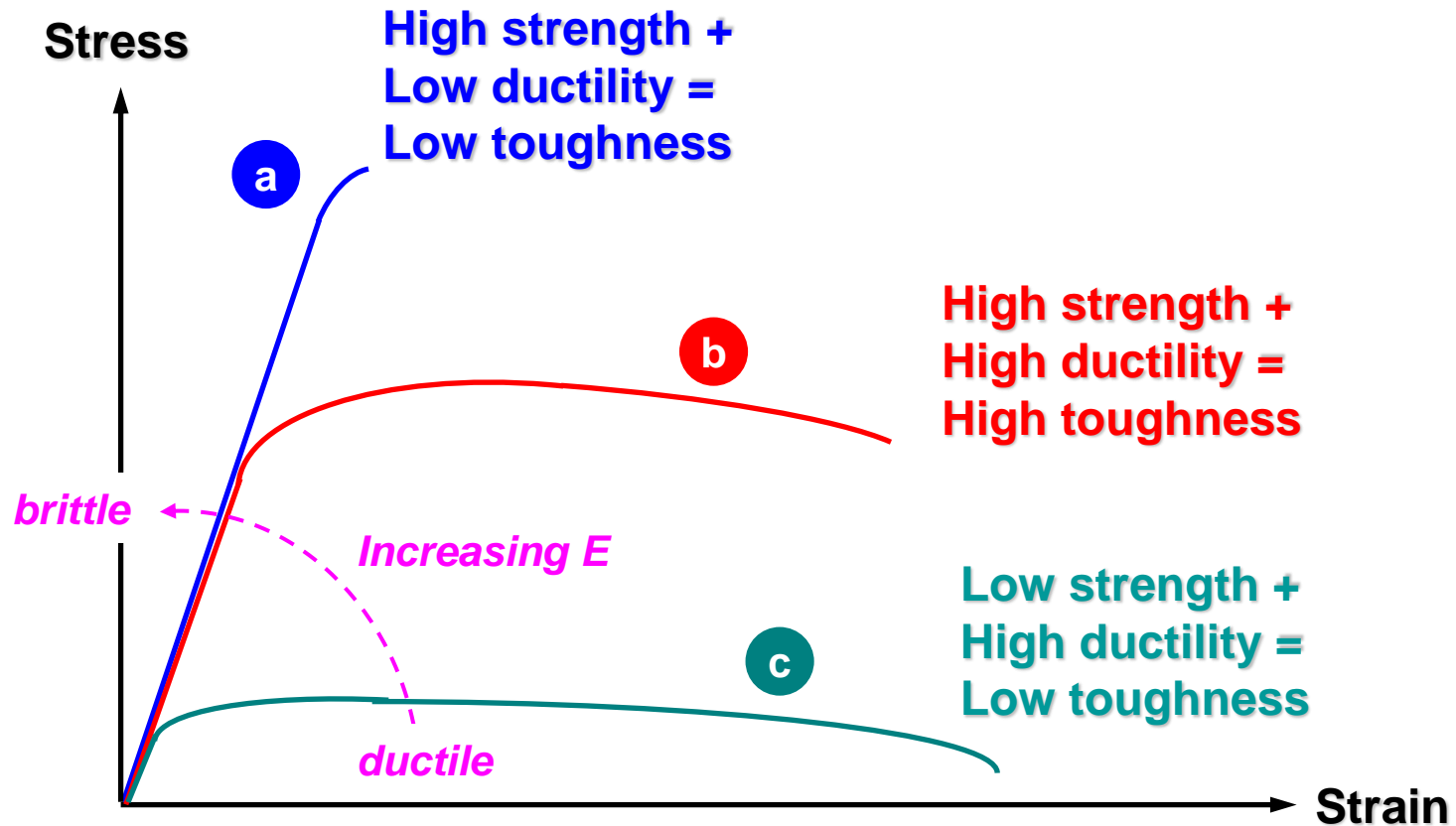
$$\%AR = \frac{(A_o - A_f)}{A_o} \times 100$$

# Toughness

- A measure of the energy needed to break a unit volume of material.
- Can be approximated by the **area under the engineering stress-strain curve**.



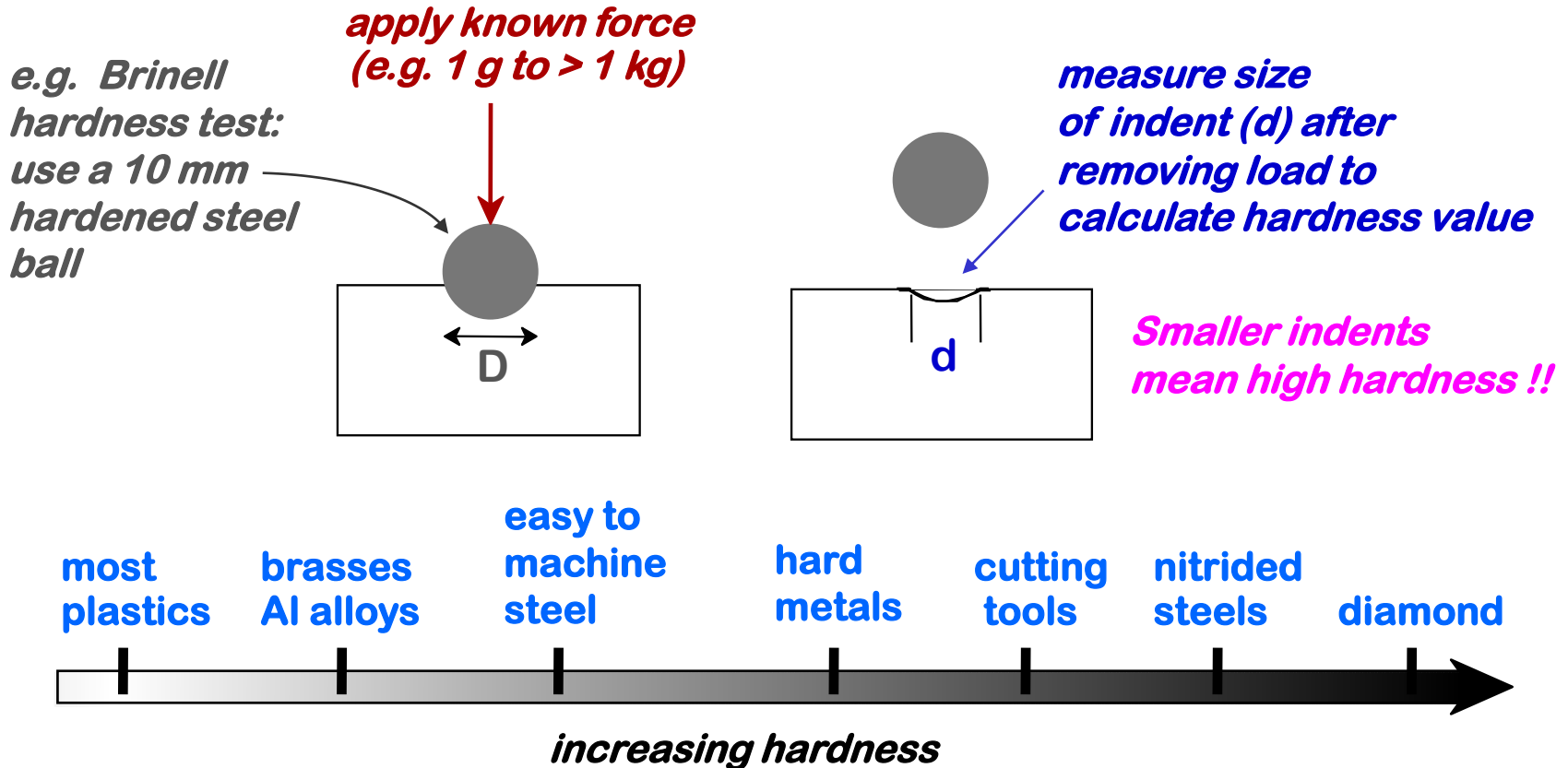
# Strength, Toughness & Ductility



- High toughness depends on the proper combination of strength and ductility
- Which material, based on their stress-strain curve shown above, is most suitable for cold working process such as rolling process?

# Hardness

- Resistance to surface scratching or indentation by another body.
- Large hardness means:
  - resistance to plastic deformation or cracking in compression
  - better wear properties (i.e. high wear resistance)





# Safety Factor (SF)

- It is impossible to perfectly analyze stresses and material properties in any design problem.
- Safety Factor (SF) is thus introduced to account for design uncertainties; the idea is to lower the working design stress limit.
- The yield stress ( $\sigma_y$ ) is normally taken as the **maximum design limit** and **NOT** the UTS since at the UTS severe plastic deformation had taken place.
- Engineers will not design components to work at the design limit but at a safe limit which is lower than the yield stress.
- Thus the **safe working design stress** ( $\sigma_{\text{working}}$ ) can be found as follow:

$$\sigma_{\text{working}} = \frac{\sigma_y}{\text{SF}}$$

- *SF may vary depending on the design requirements, from 1 to 5*
- *(SF)<sub>ave.</sub> may be taken as 2*

# Safety Factor (SF)

$$\sigma_{\text{working}} = \frac{\sigma_y}{\text{SF}}$$

*Selection of SF is based upon:*

- Previous experience
- Accuracy for which mechanical properties & material properties can be determined
- Consequences of failure in terms of loss of life, and/or property damage
- Economics & cost considerations

## ***Designing using low SF:***

- Safety may not be an issue based on past experiences or the design itself
- Select materials with small variability of properties (may incur high cost)
- Increase routine inspections to detect incipient failures

## ***Designing using high SF:***

- When safety is of ultimate concern
- High cost
- Inspection are not routine

## Example

A tensile stress is to be applied along the long axis of a cylindrical brass rod that has a diameter of 10 mm. Determine the magnitude of the load required to produce a  $2.5 \times 10^{-3}$  mm change in diameter if deformation is entirely elastic.

Take for brass:  $\mu = 0.34$  and  $E = 97$  GPa

**Solution:**

Given:  $d_o = 10$  mm ;  $\Delta d = -2.5 \times 10^{-3}$  mm ;  $\mu = 0.34$  ;  $E = 97$  GPa or  $97 \times 10^3$  MPa

→ strain in y-dir. or **lateral strain**:  $\epsilon_y = \Delta d / d_o = (-2.5 \times 10^{-3}) / (10) = -2.5 \times 10^{-4}$

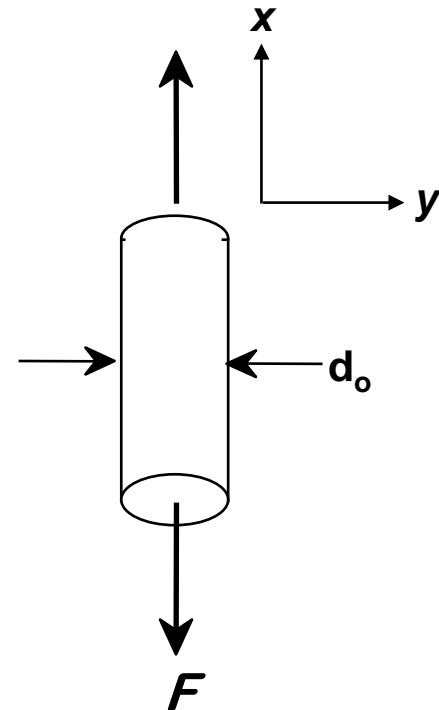
→ strain in x-dir. or **axial strain** ( $\epsilon_x$ ) can be found from:

$$\mu = -\frac{\epsilon_y}{\epsilon_x} \rightarrow 0.34 = -\frac{-2.5 \times 10^{-4}}{\epsilon_x} ; \therefore \underline{\epsilon_x = 7.35 \times 10^{-4}}$$

→ To find applied force (F):

$$E = \frac{\sigma_x}{\epsilon_x} = \frac{F}{A_o \epsilon_x} \rightarrow 97 \times 10^3 \text{ MPa} = \frac{F}{\pi \left( \frac{10 \text{ mm}}{2} \right)^2 (7.35 \times 10^{-4})}$$

$$\therefore \underline{F = 5600 \text{ N or } 5.6 \text{ kN}} \quad (\text{ans.})$$



## Example

For a bronze alloy ( $E = 115 \text{ GPa}$ ), the stress at which PD begins is  $275 \text{ MPa}$ .

- (a) What is the maximum load that may be applied to a specimen with a CSA of  $325 \text{ mm}^2$  without experiencing plastic deformation?
- (b) If the original specimen length is  $115 \text{ mm}$ , what is the maximum length to which it may be stretched without causing plastic deformation?

**Solution:**

Given:  $\sigma_y = 275 \text{ MPa}$  ;  $A_o = 325 \text{ mm}^2$  ;  $L_o = 115 \text{ mm}$  ;  $E = 115 \text{ GPa}$  or  $115 \times 10^3 \text{ MPa}$

(a) Since SF is not specified, take  $\sigma_y$  as the working limit.

To find F:

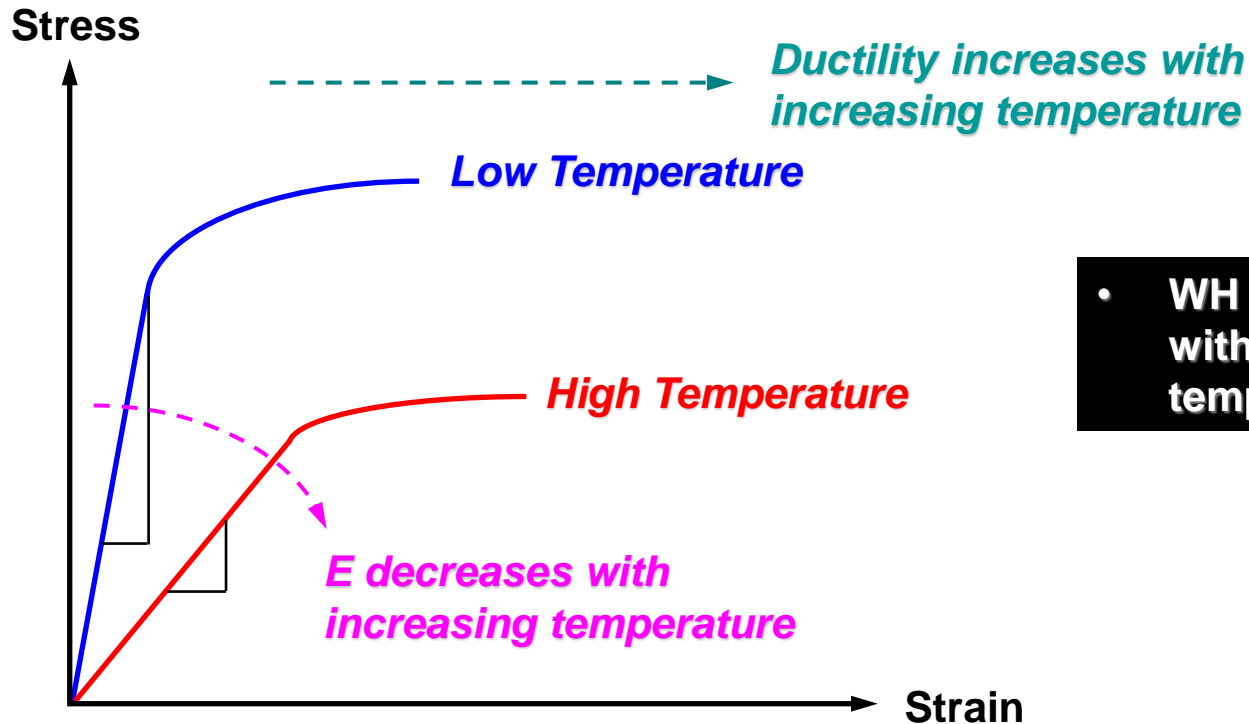
$$\sigma_y = \frac{F}{A_o} \rightarrow 275 \text{ MPa} = \frac{F}{325 \text{ mm}^2} ; \therefore \underline{F = 89,375 \text{ N or } 89 \text{ kN}} \text{ (ans.)}$$

(b) To find  $L_f$  before PD occurs i.e. still within the elastic limit:

$$\text{Elastic ext., } \delta = \frac{FL_o}{A_o E} = \frac{(89,375 \text{ N})(115 \text{ mm})}{(325 \text{ mm}^2)(115 \times 10^3 \text{ MPa})} = 0.275 \text{ mm}$$

$$\therefore L_f = L_o + \delta = 115 + 0.275 = \underline{115.275 \text{ mm}} \text{ (ans.)}$$

# Temperature Effect on Young's Modulus & Ductility



- WH also decreases with increasing temperature !

- Mechanical properties such as  $\sigma_y$ , UTS and  $E$  are temperature dependent.
- These properties decreased with increasing temperature !  
→ Reason: distance of atom or ion separation  $\uparrow$  with temperature, resulting in a decrease in inter-atomic forces between adjacent atoms or ions.
- Ductility increases with temperature.

# Summary

- **Stress** and **strain**: These are **size-independent** measures of load and displacement, respectively.
- **Elastic** behavior: This reversible behavior often shows a linear relation between stress and strain.
- To minimize deformation, select a material with a large elastic modulus (E or G).
- **Plastic** behavior: This permanent deformation behavior occurs when the tensile (or compressive) uniaxial stress reaches  $\sigma_y$ .
- **Toughness**: The energy needed to break a unit volume of material.
- **Ductility**: The plastic strain at failure.

# Resources

- Callister  
Chapter 6

**THANK YOU FOR  
YOUR ATTENTION 😊**